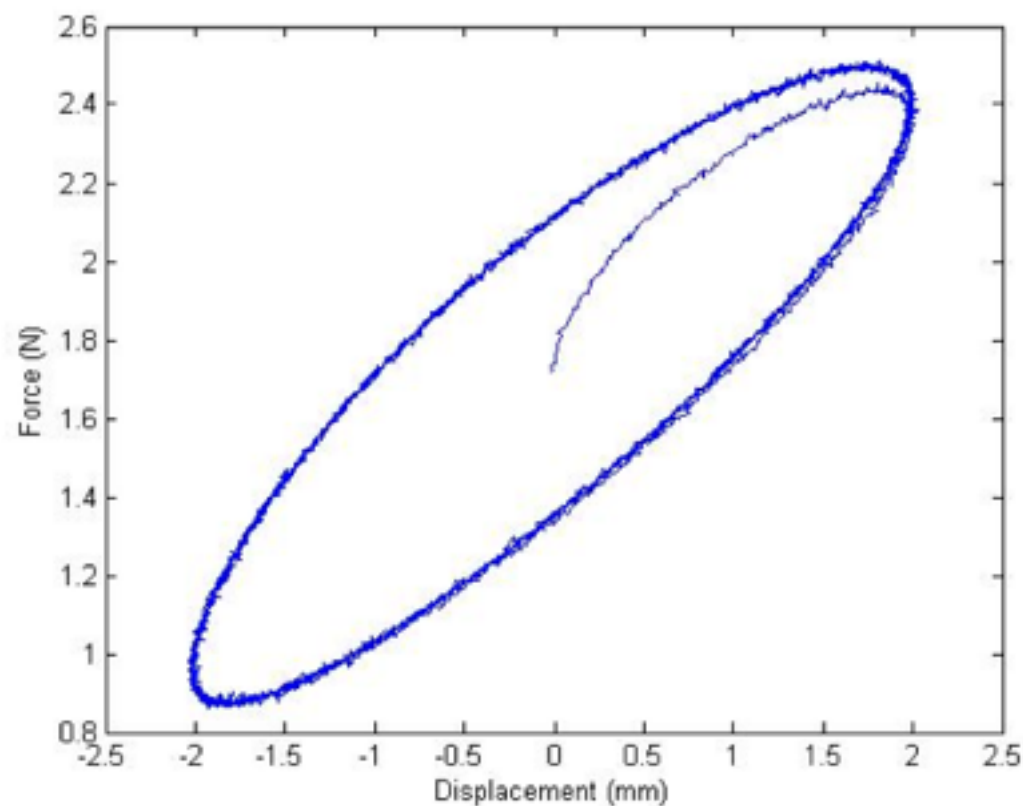


# Hysteresis of EAP

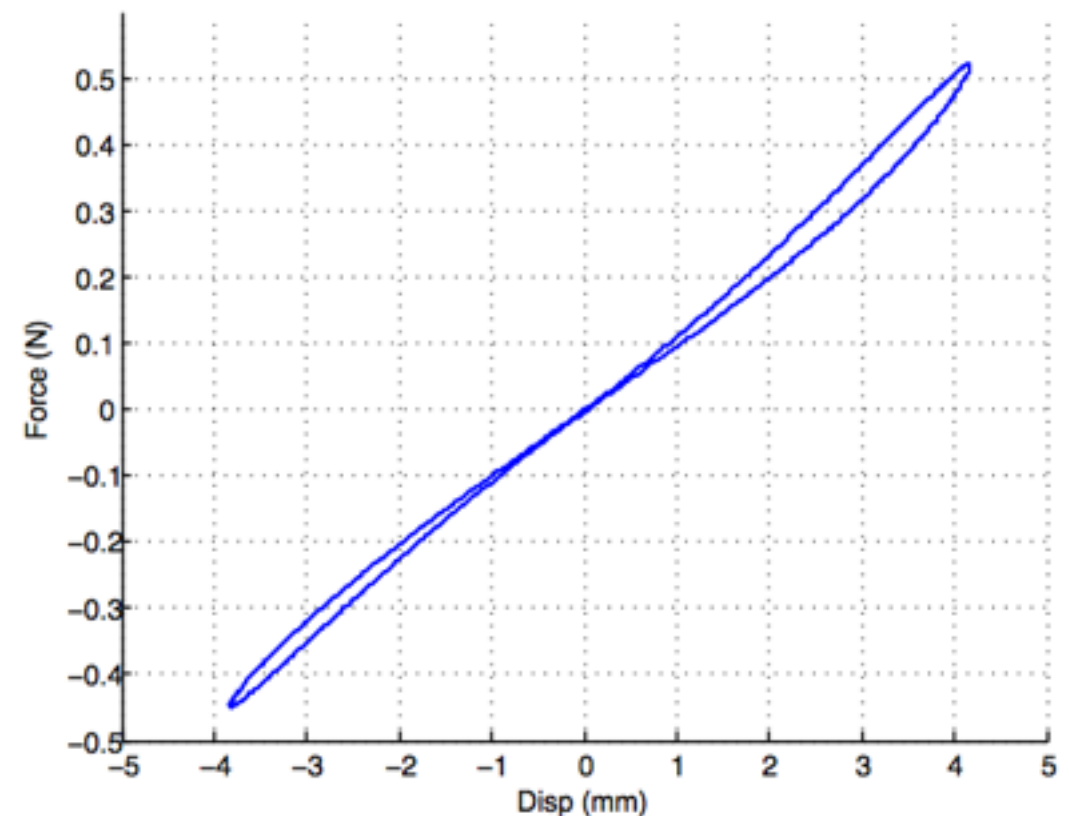
Brief Introduction  
Shiquan

# Two Configurations Tests

- Mainly because of viscoelasticity of EAP (Previous report has detailed discussion)
- Average strain change rate in the tests:
  - Planar: 33.4/s    Diaphragm: 7.7/s



Planar



Diaphragm

# Viscoelasticity of EAP

- Basically Spring + Damping
- Highly depends on strain change rate
- Energy dissipation
- The hysteresis probably is good for the application ?
  - Impact -> big strain change rate -> large hysteresis -> energy dissipation
  - Low pass

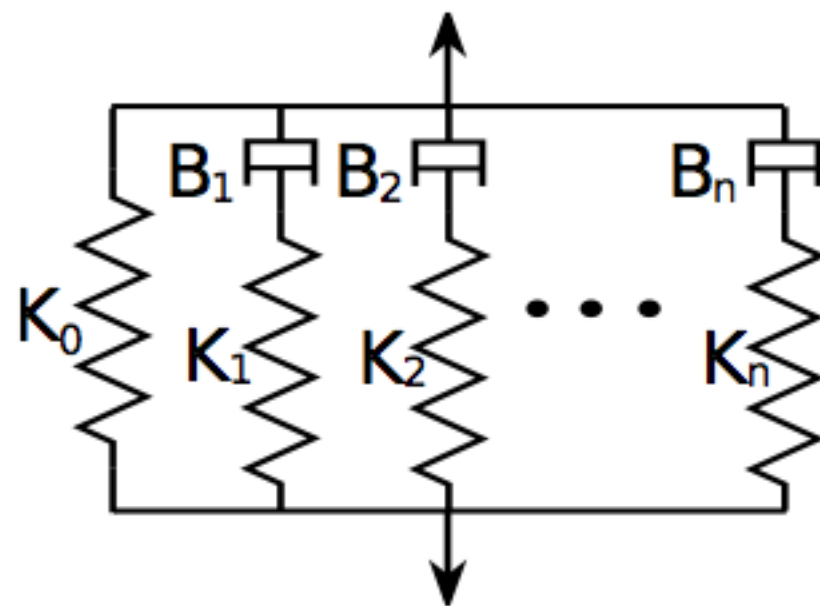
# Quasi-linear Viscoelastic (QLV) Model

- Used in Sanjay's paper and verified by experiments

- Transfer function

$$\frac{\mathbf{F}}{\mathbf{X}} = k_0 + \sum_{i=1}^n \frac{k_i s}{s + \frac{k_i}{b_i}}$$

- Related parameters:



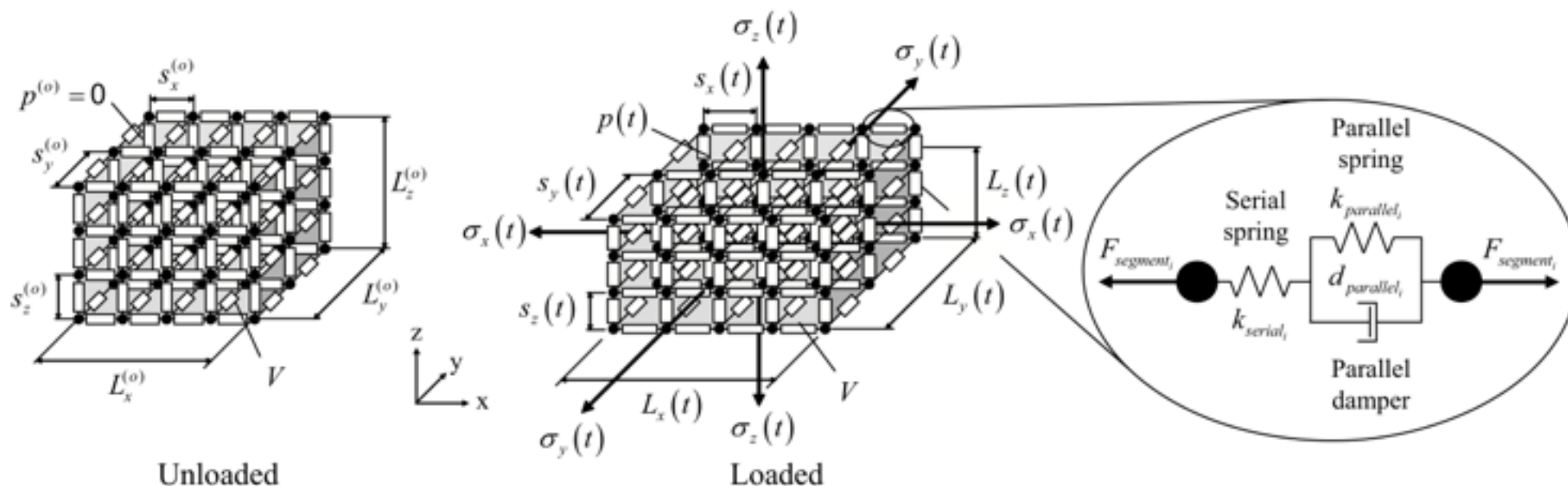
QLV Params	CV	CC
$k_0$	1.35	1.44
$k_1$	1.63	1.66
$b_1$	1.14e-2	1.22e-2
$k_2$	0.71	0.66
$b_2$	3.00 e-2	3.18e-2
$k_3$	0.29	0.48
$b_3$	0.52	0.61
$k_4$	0.37	0.50
$b_4$	0.088	0.17

# Another model :Visco-hyperelastic Film Model

- Lack of experiment verification
- Stress versus stretch ratio:

$$K_s K_p \left( \frac{1}{\sqrt{\lambda_{\text{test}}}} - 1 \right) + D_p K_s \frac{d}{dt} \left( \frac{1}{\sqrt{\lambda_{\text{test}}}} \right)$$

$K_s = 2.31 \times 10^{-2} \text{ Nmm}^{-2}$ ,  $K_p = 5.20 \times 10^{-2} \text{ Nmm}^{-2}$  and  $D_p = 3.3 \times 10^1 \text{ N s mm}^{-2}$



# References

- Dastoor, S.; Cutkosky, M.; , "Design of dielectric electroactive polymers for a compact and scalable variable stiffness device," Robotics and Automation (ICRA), 2012 IEEE International Conference on , vol., no., pp.3745-3750, 14-18
- Michael Wissler, Edoardo Mazza, Mechanical behavior of an acrylic elastomer used in dielectric elastomer actuators, Sensors and Actuators A: Physical, Volume 134, Issue 2, 15 March 2007, Pages 494-504
- Characterization of dielectric elastomer actuators based on a visco-hyperelastic film model Patrick Lochmatter et al 2007 Smart Mater. Struct. 16 477 May 2012