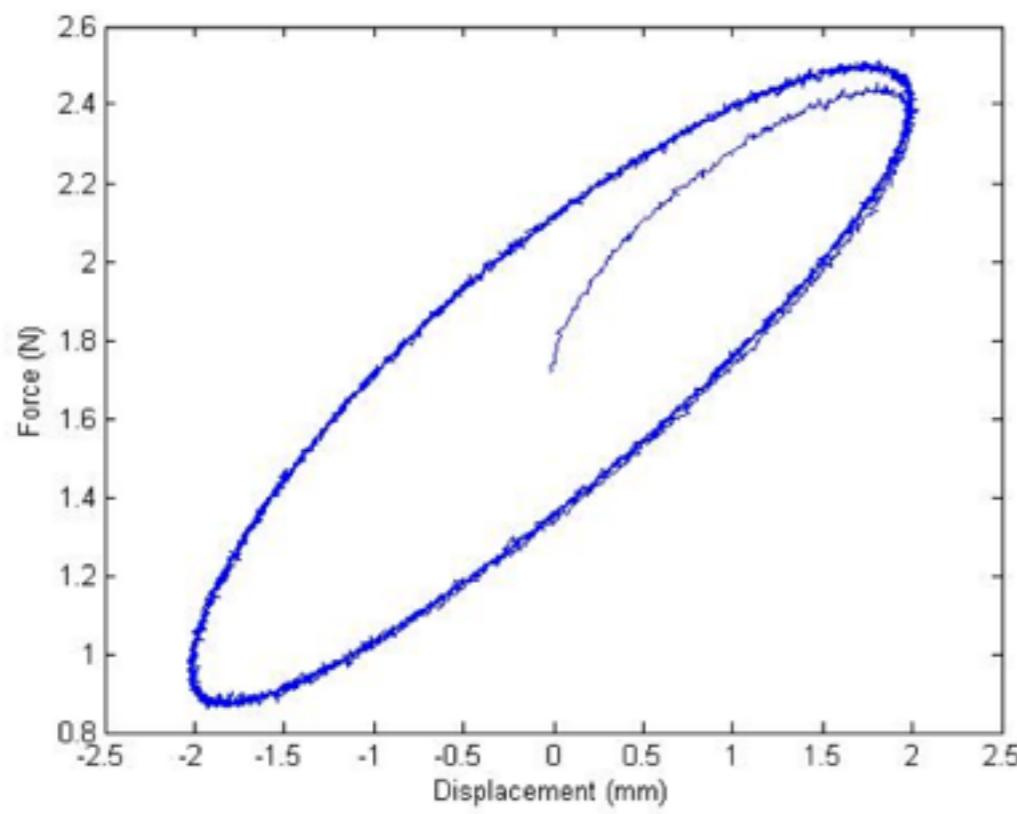


Hysteresis of EAP

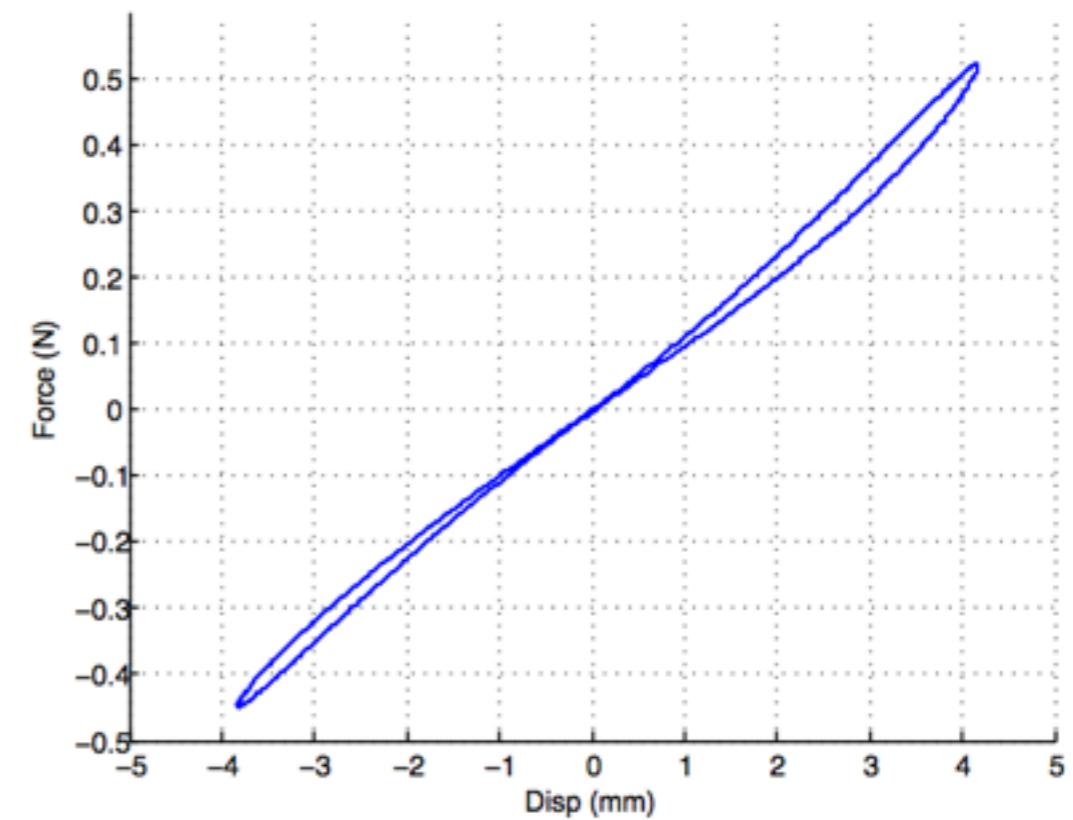
Brief Introduction
Shiquan

Two Configurations Tests

- Mainly because of viscoelasticity of EAP
(Previous report has detailed discussion)
- Average strain change rate in the tests:
 - Planar: 33.4/s Diaphragm: 7.7/s



Planar



Diaphragm

Viscoelasticity of EAP

- Basically Spring + Damping
- Highly depends on strain change rate
- Energy dissipation
- The hysteresis probably is good for the application ?
 - Impact -> big strain change rate -> large hysteresis -> energy dissipation
 - Low pass

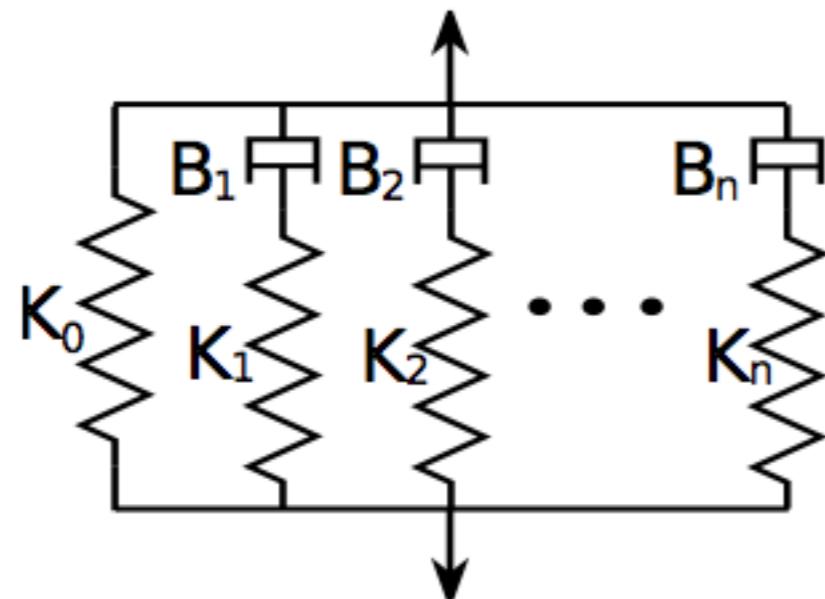
Quasi-linear Viscoelastic (QLV) Model

- Used in Sanjay's paper and verified by experiments

- Transfer function

$$\frac{F}{X} = k_0 + \sum_{i=1}^n \frac{k_i s}{s + \frac{k_i}{b_i}}$$

- Related parameters:



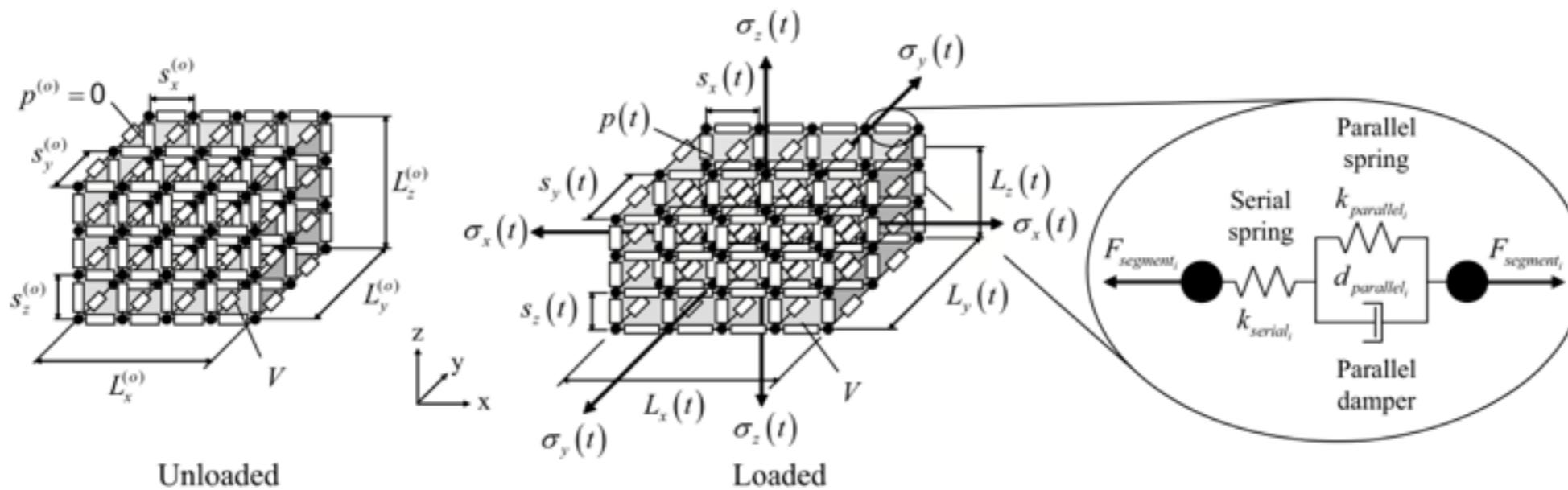
QLV Params	CV	CC
k_0	1.35	1.44
k_1	1.63	1.66
b_1	1.14e-2	1.22e-2
k_2	0.71	0.66
b_2	3.00 e-2	3.18e-2
k_3	0.29	0.48
b_3	0.52	0.61
k_4	0.37	0.50
b_4	0.088	0.17

Another model : Visco-hyperelastic Film Model

- Lack of experiment verification
- Stress versus stretch ratio:

$$K_s K_p \left(\frac{1}{\sqrt{\lambda_{\text{test}}}} - 1 \right) + D_p K_s \frac{d}{dt} \left(\frac{1}{\sqrt{\lambda_{\text{test}}}} \right)$$

$K_s = 2.31 \times 10^{-2} \text{ Nmm}^{-2}$, $K_p = 5.20 \times 10^{-2} \text{ Nmm}^{-2}$ and $D_p = 3.3 \times 10^1 \text{ N s mm}^{-2}$



References

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- Michael Wissler, Edoardo Mazza, Mechanical behavior of an acrylic elastomer used in dielectric elastomer actuators, Sensors and Actuators A: Physical, Volume 134, Issue 2, 15 March 2007, Pages 494-504
- Characterization of dielectric elastomer actuators based on a visco-hyperelastic film modelPatrick Lochmatter et al 2007 Smart Mater. Struct. 16 477May 2012